



Solar Imaging Radio Array (*SIRA*)

Flight Dynamics

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August 28, 2003



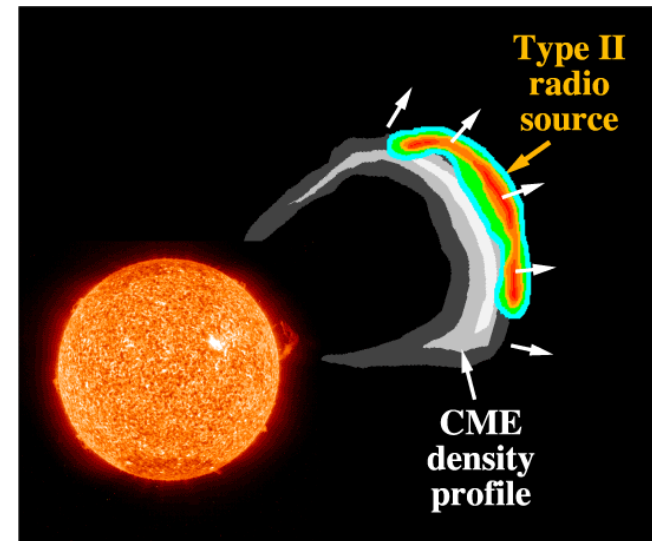


Solar Imaging Radio Array (SIRA) Trajectory and Formation Analysis

Integrated Design Capability / Integrated Mission Design Center

Agenda

- Mission Metrics
- Orbit Trades
 - Orbit Options
 - Shadows
 - Coverage
 - Launch Options
- Formation Control
- Summary
- Other Orbits



Two dimensional radio imaging of the CME-driven shock front and the CME density profile is critical for predicting the space weather effects of CMEs





SIRA Metrics

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- Earth-constellation distance: $> 50 R_e$ (less interference) and $< 100 R_e$ (link margin).
 - **Closer than 100 Re would be desirable to improve the link margin requirement**
 - **A retrograde orbit of $< 160 R_e$ (10^6 km), for a stable orbit would be ok**
- The density of "baselines" in the u-v plane should be uniformly distributed. Satellites randomly distributed on a sphere will produce this result.
- Formation diameter: ~ 25 km to achieve desired angular resolution
- The plan is to have up to 16 microsats, each with its own "downlink".
- Satellites will be "approximately" 3-axis stabilized.
- Lower energy orbit insertion requirements are always appreciated.
- Eclipses should be avoided if possible.
- Defunct satellites should not "interfere" excessively with operational satellites.





SIRA Orbit Selection Trade

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	DRO-TB	DRO-Lunar	Earth-Moon Lib	Sun-Earth Lib
Launch C3 Energy (km ² /s ²)	-0.1	-0.1	-1.8	-0.67
Mission Orbit Insertion ΔV (m/s)	3 to 200	416	700	~10
Orbit Maintenance ΔV/year (m/s)	0	0	5	5
Formation Maintenance ΔV/month (m/s) per spacecraft Strict (S) & Loose (L), Assuming 0.1mN	S – 1.32 L – 0.70	S – 1.32 L – 0.70	S – 1.30 L - 0.69	S – 0.052 L – 0.024
Min / Max Distances to Earth (10 ⁶ km)	0.5 to 7.0	0.5 only	0.25 to 0.5	1.2 to 1.7
Shadows	None	None for 3 years 9 min lunar penumbra in 4 th year	None	None
Angle variation between Spacecraft-Earth and Spacecraft-Sun vectors over one orbit period (degrees)	360.	360.	360.	+/-37.0

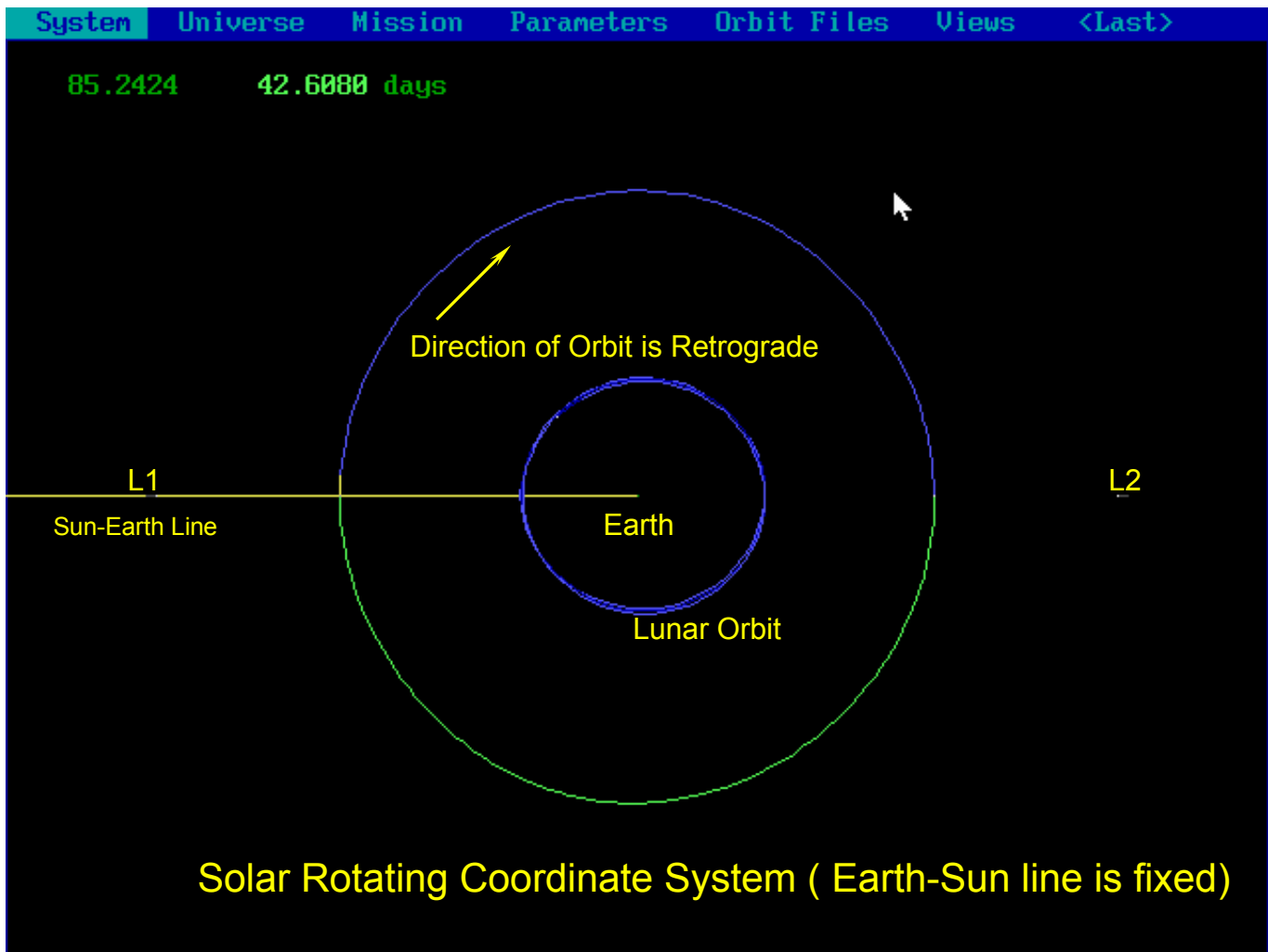
TB= Three Body Dynamics





SIRA Retrograde Orbit

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Why RO?

- Stable Orbit
- No Stationkeeping Delta-V
- Not as distant as L1
- Multiple Transfers
- No Shadows?
- Good Environment
- ✓ Really a Lunar Periodic Orbit
- ✓ Classified as a Symmetric Doubly Asymptotic Orbit in the Restricted Three-Body Problem





SIRA Orbit Options- Near Retrograde Orbit Lunar Transfer

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Transfer Type	Lunar Gravity Assist	Lunar Gravity Assist	Lunar Gravity Assist	Lunar Gravity Assist
Transfer Time to Mission Orbit (days)	6	7	4.5	8
Inclination to Ecliptic Plane (deg)	23	18	8	2
Initial Orbit Radius (km)	460,000	495,000	425,000	553,000
Initial Period (days)	36.0	40.1	31.9	47.3
Final Orbit Radius (km)	445000 x 510,000	475000 x 515,000	425000 x 481,000	530000 x 583,000
Final Period (days)	38.0	40.2	35.1	47.8
Transfer Injection C3 (km ² /s ²)	0.046	0.135	-0.291	-0.230
Mission Orbit Injection ΔV (m/s)	403	416	495	520

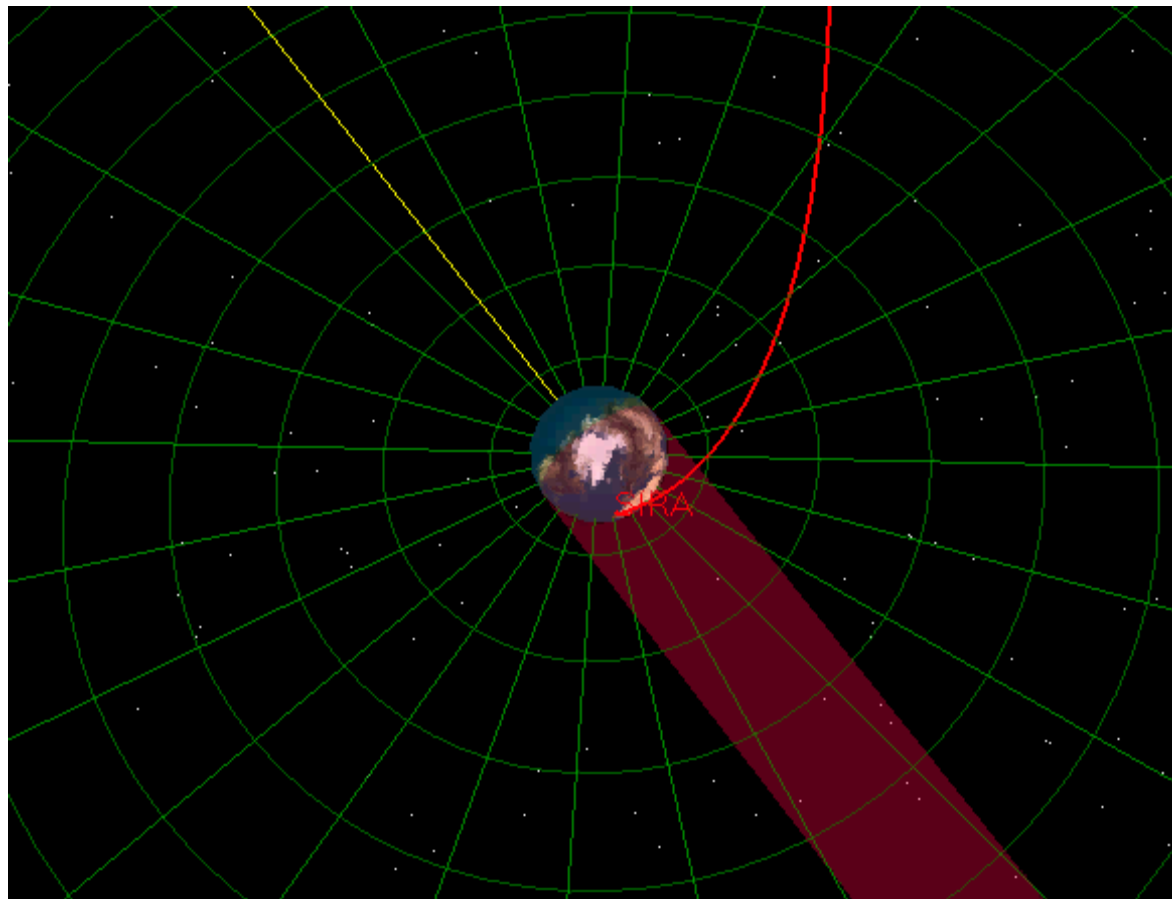
Note: Lunar Gravity Assist distance approx 3200km from lunar center
No Stationkeeping maneuvers required for NRO





SIRA Orbit Options – Lunar Transfer and Final Orbit

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SIRA Orbit Options –Shadow and Coverage

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Shadow

Orbit Radius (km)	460,000	495,000	425,000	553,000
Inclination to Ecliptic Plane (deg)	23	18	8	2
Final Orbit Period (days)	38.0	40.2	35.1	47.8
Shadow in Mission Orbit	None for 4 years	None for 3 years 9 min lunar penumbra in 4 th year	0.5 hr. lunar umbra in 1 st year 2 hr. Earth umbra in 3 rd year Multiple penumbra events	No umbra for 1 st 2 years 2-3 1-2 hr. umbra in 3 rd and 4 th year Multiple penumbra events

Coverage

Initial Orbit Radius (km)	460,000	495,000	425,000	553,000
Inclination to Ecliptic Plane (deg)	23	18	8	2
Final Period (days)	38.0	40.2	35.1	47.8
DSN Coverage Gaps in Mission Orbit	215 hours over 4 years	110 hours over 4 years	8 hours over 4 years	Continuous Coverage





SIRA Navigation

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Navigation

- Traditional ground orbit determination for the carrier and for each spacecraft. X-band Downlink
- Additional measurement data of inter-spacecraft range information
- Anticipated accuracies of ~ 3 m inter-spacecraft range and < 100 m absolute position.

Tracking data coverage requirements:

- Launch and early orbit: 12 hrs
- Cis-lunar: 8 hours every day to perilune
- Post-lunar: 12 hrs for insertion maneuver plan
- Deployment: TBD
- Mission Orbit and formation maintenance: several hrs per day on each spacecraft for 1st week.
- Several hours per week thereafter





SIRA Formation Analysis

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- Formations are all baselined to maintain a sphere of 25 km radius.
 - Center of sphere was placed onto orbit
 - Constant low thrust control assuming 0.1mN
 - Simple PD controller to hold position
- A sphere was used for initial placement of formation spacecraft.
 - A uniformly distributed sphere was computed using Robert Bauer's "Uniform Sampling of SO3" algorithm from 2001 Flight Mechanics Symposium"
 - Spacecraft location on sphere held with respect to each other
 - A strict and a loose formation control was then applied.





SIRA Formation Control Analysis

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How much ΔV to initialize, maintain, and resize?

Phase	Max	Mean	Min	Std
	[m/s]	[m/s]	[m/s]	[m/s]
a	0.635	0.607	0.592	0.014
b	1.323	0.792	0.392	0.293
c	0.757	0.674	0.541	0.069
d	0.679	0.616	0.582	0.031
e	1.201	0.721	0.367	0.263
f	0.679	0.608	0.503	0.056
Phase Description				
a) Init 25km sphere				
b) Maintain 25km sphere (strict PD control) one month				
c) Maintain 25km sphere (loose control) one month				
d) Resize from 25km to 50km				
e) Maintain 50km sphere (strict PD control) one month				
f) Maintain 50km sphere (loose control) one month				

Examples:

Initialize & maintain 2 yr:
= 33 m/s

Initialize, Maintain 2yr,
& four resizes:
= 36 m/s





SIRA Trade Summary

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- Given mission metrics and assumptions, analysis shows feasibility of SIRA mission with a spherical formation
- Chosen lunar transfer ΔV is < 500 m/s and is dependent upon orbit distance and lunar assist conditions
- Formation Initialization, maintenance, and resize in general is not a driver; possible ΔV requirement of ~ 36 m/s
 - **Formation Maintenance ΔV /month (m/s) < 1.5 m/s**
 - **Initialization ΔV (m/s) < 1 m/s**
 - **Resize ΔV (m/s) < 1 m/s**
 - **Additional analysis required for maneuver type and system engineering aspects**
- Orbit selection dependent upon mission metrics, launch mass capability, system engineering





Considerations for Future Orbit Analysis

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- Shadows are seasonally dependent
- Final mission orbit is geometry dependent on cis-lunar trajectory, epoch, parking orbit, and lunar inclination
- Launch windows of approximately 5 days with moon perpendicular to Sun-Earth line
- Launch vehicle error correction of approx 50 m/s
- Re-contact analysis
- Selection of natural dynamics to minimize formation control effort
- Navigation on each s/c after deployment
- Navigation for post launch (12 hrs), post gravity assist / pre-insertion (12 hrs), and deployment (TBD hrs)
- Formation deployment / initialization and maintenance maneuver modeling - Initialization and control effort combined with finite maneuver planning / propulsion design
- Inter-spacecraft timing transfer synchronization





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Backup





SIRA Orbit Selection Trade

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- A brief orbit trade was performed for the SIRA mission based on metrics
- Three orbits were reviewed,
 - ✓ Earth-Moon L4 Libration orbit
 - ✓ Earth Centered Retrograde orbits (lunar transfer and three body transfer)
 - ✓ Sun-Earth L1 Libration orbit
- All orbit trades used high fidelity perturbation modeling and precision integrators
- A moon centered circular orbit at about 30,000km was also analyzed, but was eliminated due to the high insertion ΔV cost of over 1km/s.





SIRA Orbit Options – Distant Retrograde Orbit Three-body Transfer

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Transfer Type	Three-body	Three-body	Three-body	Three-body	Three-body
Final Orbit Radius (km)	500,000	750,000	900,000	1,050,000	1,200,000
Transfer Time to Mission Orbit (days)	151	231	253	282	304
Inclination to Ecliptic Plane (deg)	0 / 5	0	0	0	0 / 5
Max Transfer Distance (km) (10^6)	2.5	4.5	5.3	6.5	7.3
Initial Period (days)	39	67	86	105	122
Transfer Injection C3 (km^2/s^2)	-.13	0.02	0.10	0.15	0.26
Mission Orbit Injection ΔV (m/s)	210 / 256	43	23	7	3 / 28





SIRA Orbit Options –Shadows

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Three Body Option

Final Orbit Radius (km)	500000	750000	900000	1050000	1200000
Final Orbit Period (days)	39	67	86	105	122
Shadow in Mission Orbit (no lunar shadows)	Penumbra: 5 hrs Umbra: 2 hrs [5 deg: None]	Penumbra: 6 hrs Umbra: 2 hrs	Penumbra: 7 hrs Umbra: 2 hrs	Penumbra: 7 hrs Umbra: 1 hr	Penumbra: 8 hrs Umbra: None [5 deg: None]

Lunar Orbit Option

Orbit Radius (km)	460,000	495,000	425,000	553,000
Inclination to Ecliptic Plane (deg)	23	18	8	2
Final Orbit Period (days)	38.0	40.2	35.1	47.8
Shadow in Mission Orbit	None for 4 years	None for 3 years 9 min lunar penumbra in 4 th year	0.5 hr. lunar umbra in 1 st year 2 hr. Earth umbra in 3 rd year Multiple penumbra events	No umbra for 1 st 2 years 2-3 1-2 hr. umbra in 3 rd and 4 th year Multiple penumbra events





SIRA Orbit Options – Coverage

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Initial Orbit Radius (km)	460,000	495,000	425,000	553,000
Inclination to Ecliptic Plane (deg)	23	18	8	2
Final Period (days)	38.0	40.2	35.1	47.8
DSN Coverage Gaps in Mission Orbit	215 hours over 4 years	110 hours over 4 years	8 hours over 4 years	Continuous Coverage





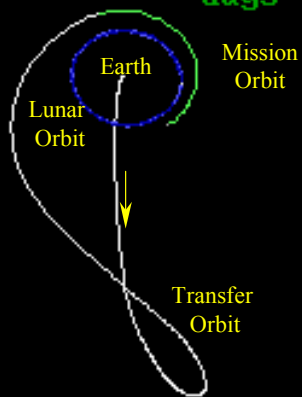
SIRA Orbit Options – Three Body Transfer and Final Orbit

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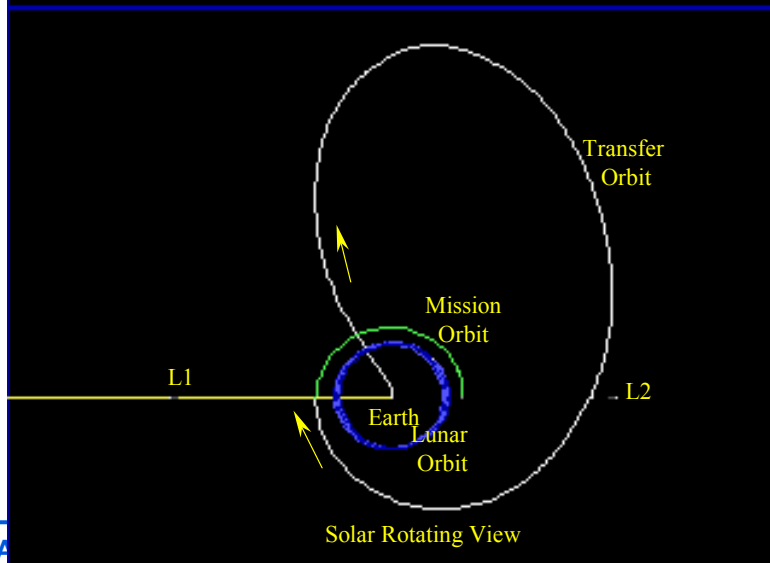
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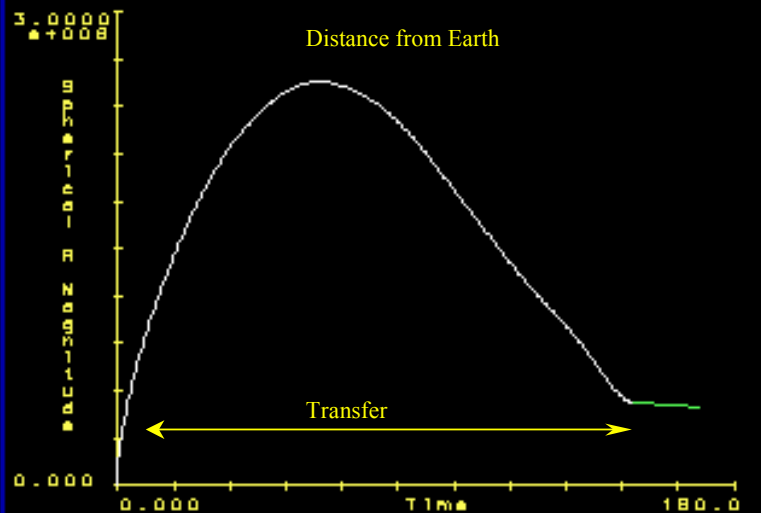
days



EarthGCI View



Solar Rotating View



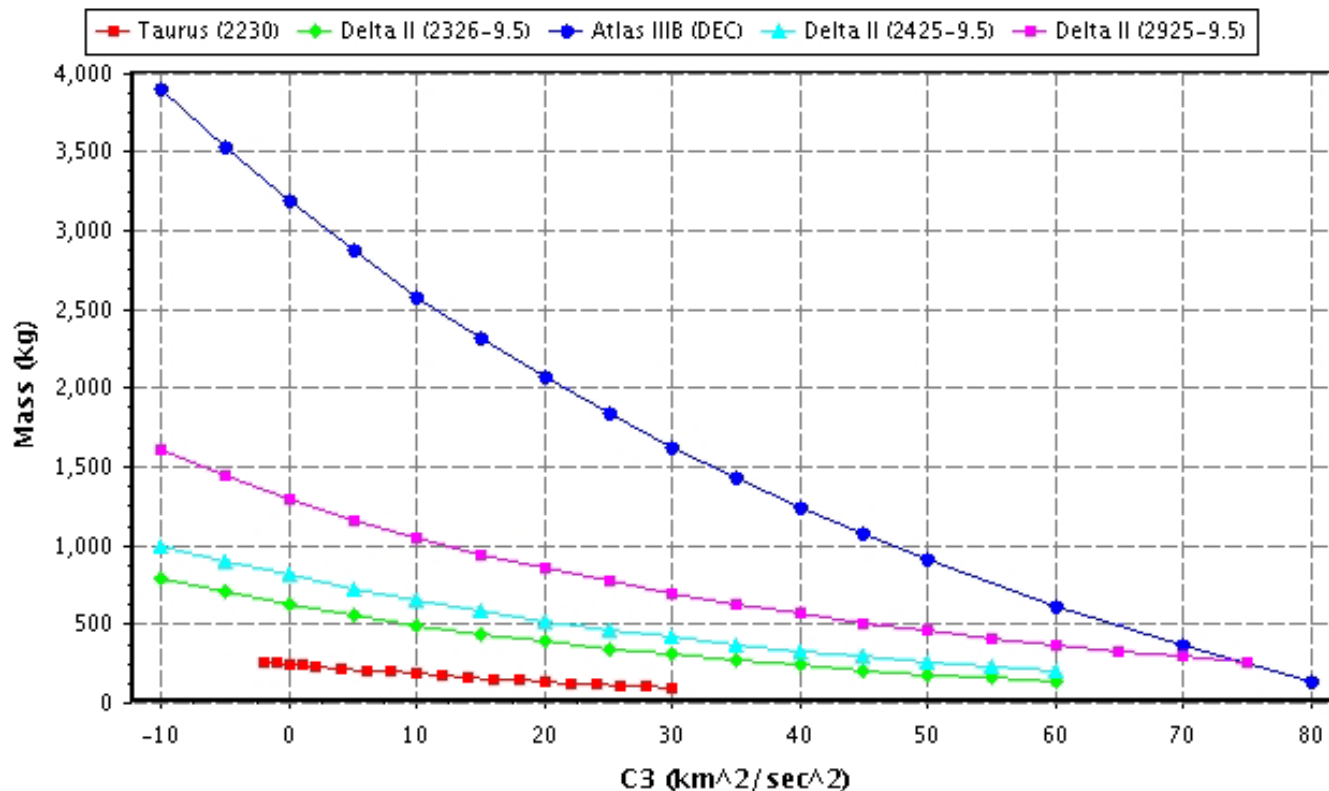


SIRA Orbit Options – Launch

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Important Note: The data contained in these curves are based on ground rules and assumptions located below the plot. Please read this information carefully. This information is intended for NASA customers only.

NASA ELV Performance Estimation Curve(s)
High Energy Orbits
Please note ground rules and assumptions below.





SIRA Orbit Options – Launch

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Launch vehicle payload mass capabilities for a $C3 \sim 0 \text{ km}^2/\text{sec}^2$, from ELV web site

Taurus (2230)	245.0		
Taurus (2130)	295.0	Delta II (2926-9.5)	1140.0
Delta II (2326-10)	600.0	Delta II (2925-10L)	1225.0
Delta II (2920-10L)	620.0	Delta II (2925-10)	1240.0
Delta II (2920-10)	625.0	Delta II (2925-9.5)	1290.0
Delta II (2326-9.5)	625.0	Delta II (2926H-10L)	1305.0
Delta II (2920-9.5)	690.0	Delta II (2926H-10)	1315.0
Delta II (2426-10)	695.0	Delta II (2926H-9.5)	1345.0
Delta II (2426-9.5)	715.0	Delta II (2925H-10L)	1480.0
Delta II (2425-10)	790.0	Delta II (2925H-10)	1495.0
Delta II (2425-9.5)	810.0	Delta II (2925H-9.5)	1525.0
Delta II (2920H-10L)	860.0	Delta III (3940-11)	2625.0
Delta II (2920H-10)	875.0	Atlas IIIB (SEC)	2975.0
Delta II (2920H-9.5)	905.0	Atlas IIIB (DEC)	3180.0
Delta II (2926-10L)	1075.0		
Delta II (2926-10)	1085.0		



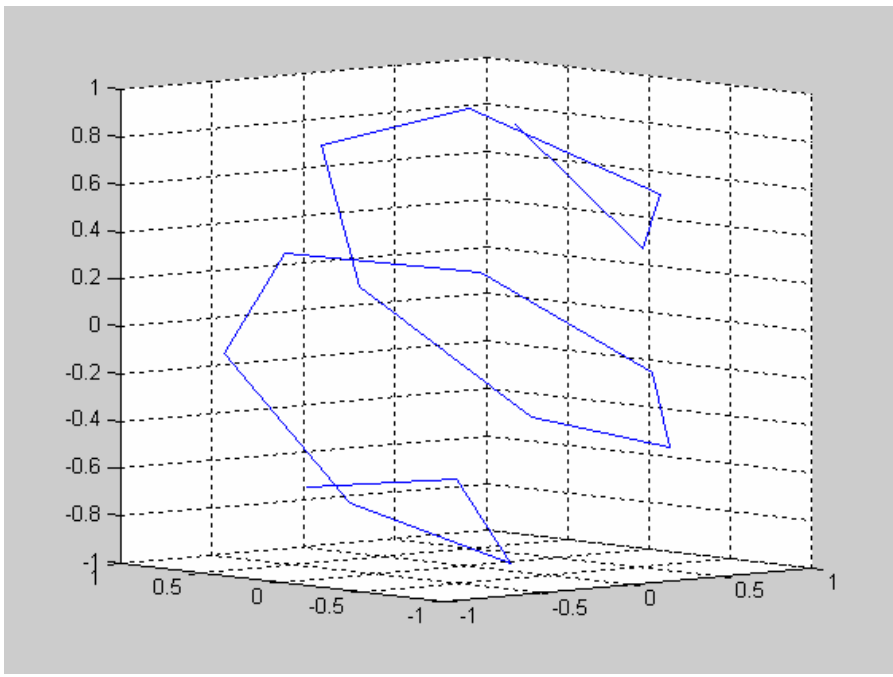


SIRA Formation Analysis

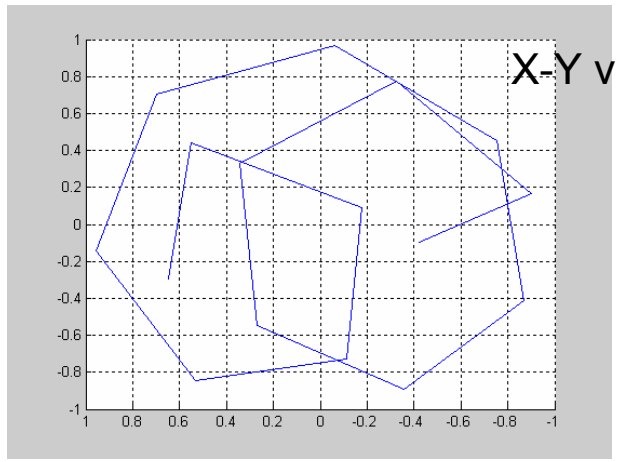
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- Matlab generated sphere based on S03 algorithm
 - ✓ Uniform distribution of points on a unit sphere
 - ✓ 16 points at vertices represents spacecraft locations

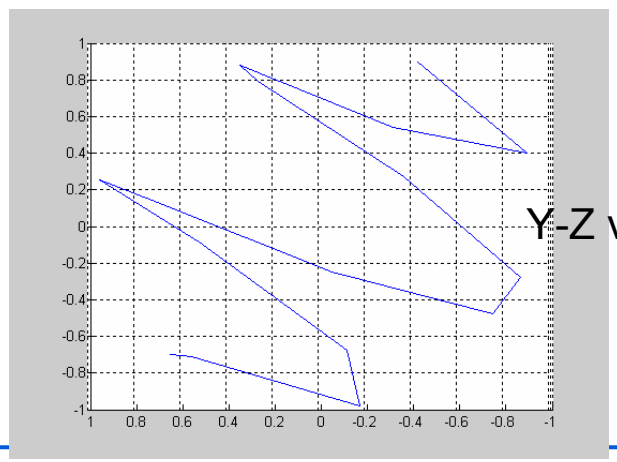
3-D view



X-Y view



Y-Z view





SIRA Formation Control Analysis

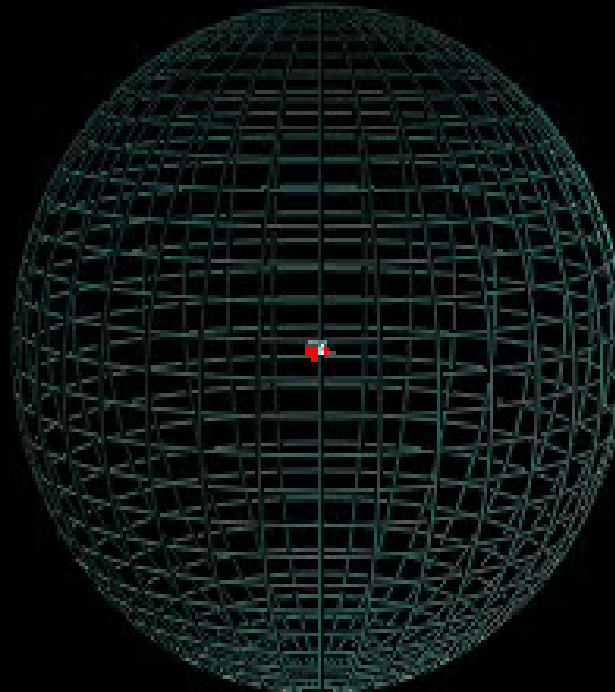
Integrated Design Capability / Integrated Mission Design Center

Jan 01 2005 12:04:27.965

Target: A1

Source: A1(270° RA, 10° Dec, 175 km Radius)

FOV: 25°





SIRA Formation Control Analysis

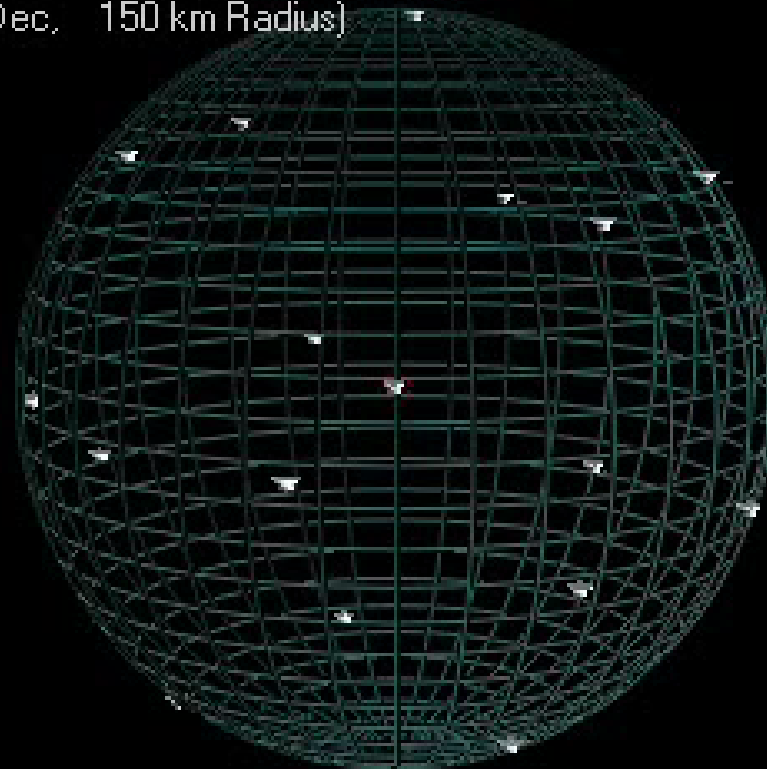
Integrated Design Capability / Integrated Mission Design Center

Jan 01 2005 12:04:27.965

Target: A1

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FOV: 25°





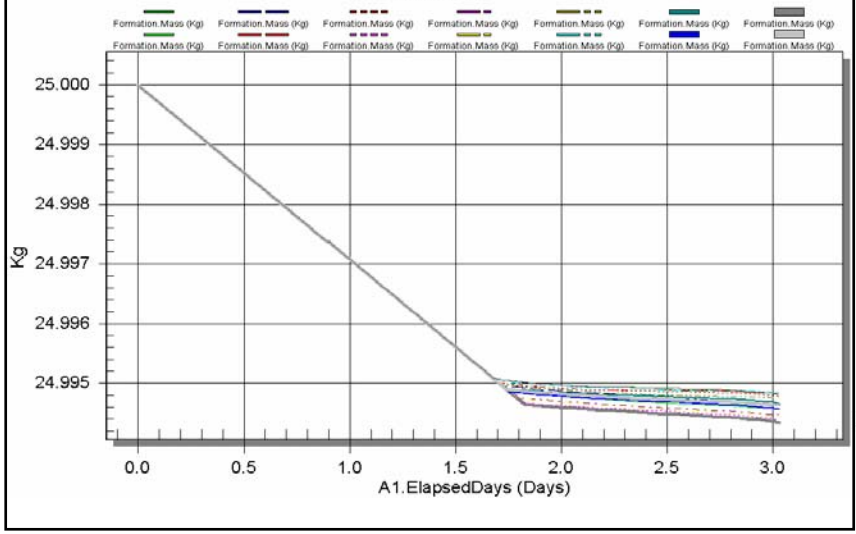
SIRA Formation Control Analysis

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- Initialization and maintenance
- Spacecraft controlled to maintain only relative separations
- Plots show formation position and drift (sphere represent 25km radius)
- Maneuver performed in most optimum direction based on controller output

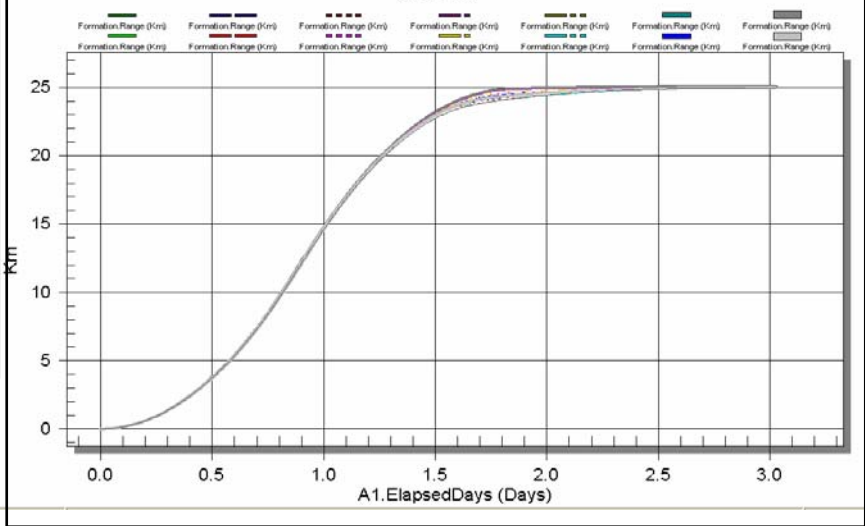
Mass Depletion

FreeFlyer Plot Window
8/22/2003



Radial Distance from Center

FreeFlyer Plot Window
8/22/2003



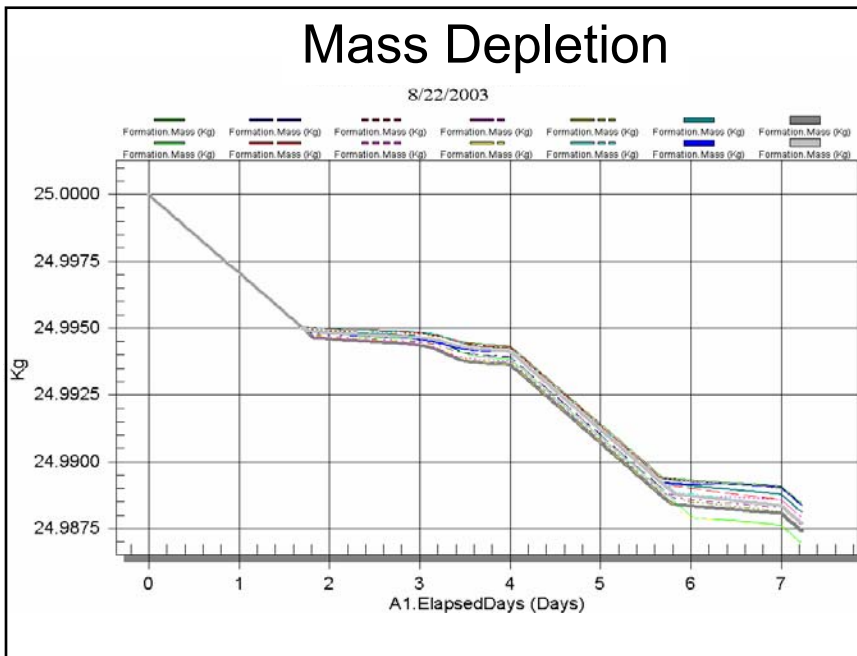


SIRA Formation Control Analysis

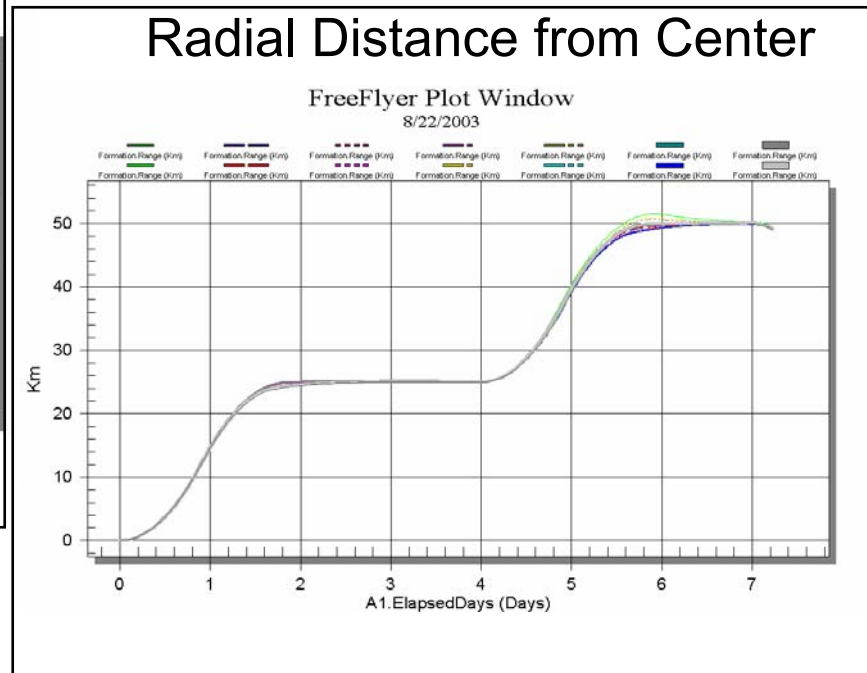
Integrated Design Capability / Integrated Mission Design Center

- Initialization, maintain, resize, maintain
- Spacecraft controlled to maintain only relative separations
- Maneuver performed in most optimum direction based on controller output

Mass Depletion



Radial Distance from Center

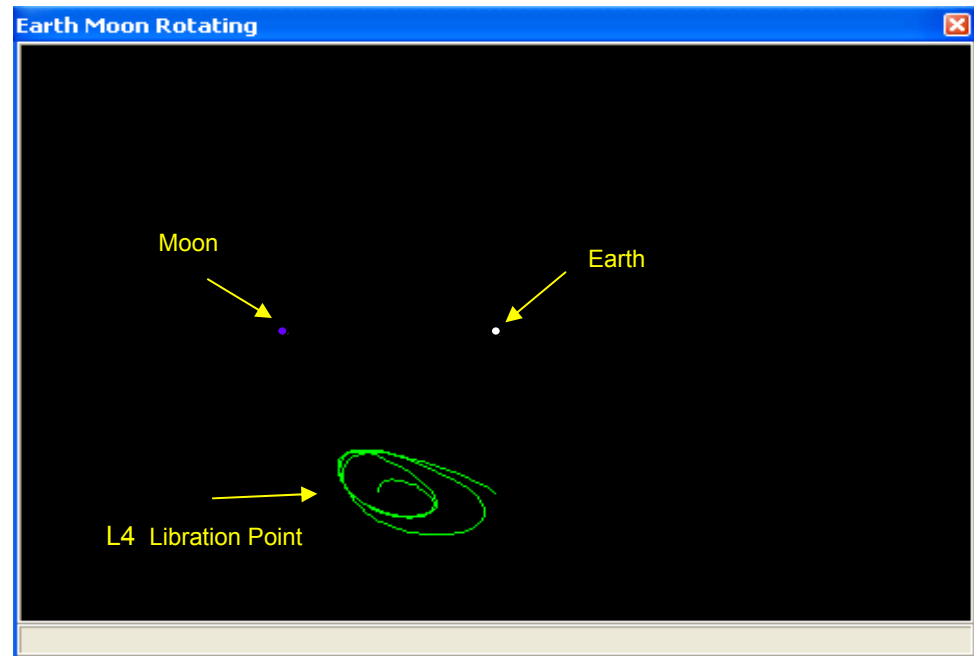
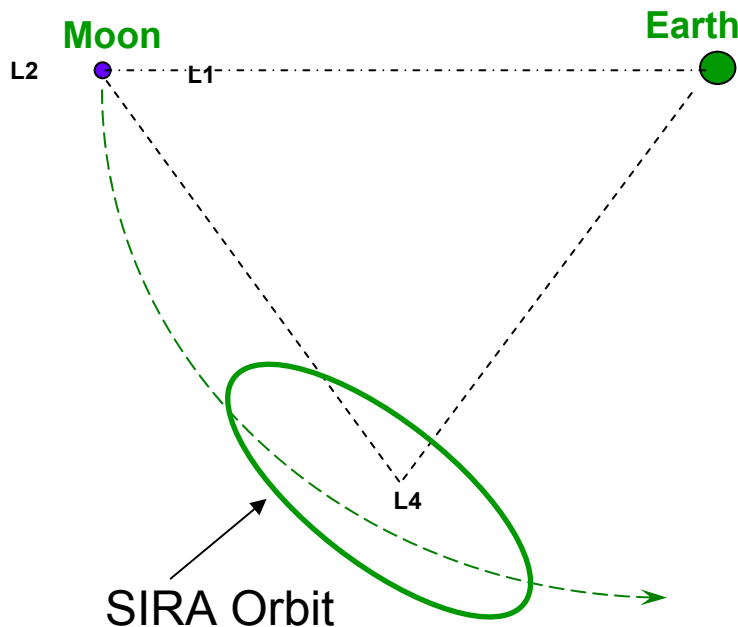




Earth - Moon L4 Libration Orbit

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- Stable orbit in Earth - moon neighborhood
- L4 Location is at equal distances from Earth and Moon
- Requires insertion maneuver



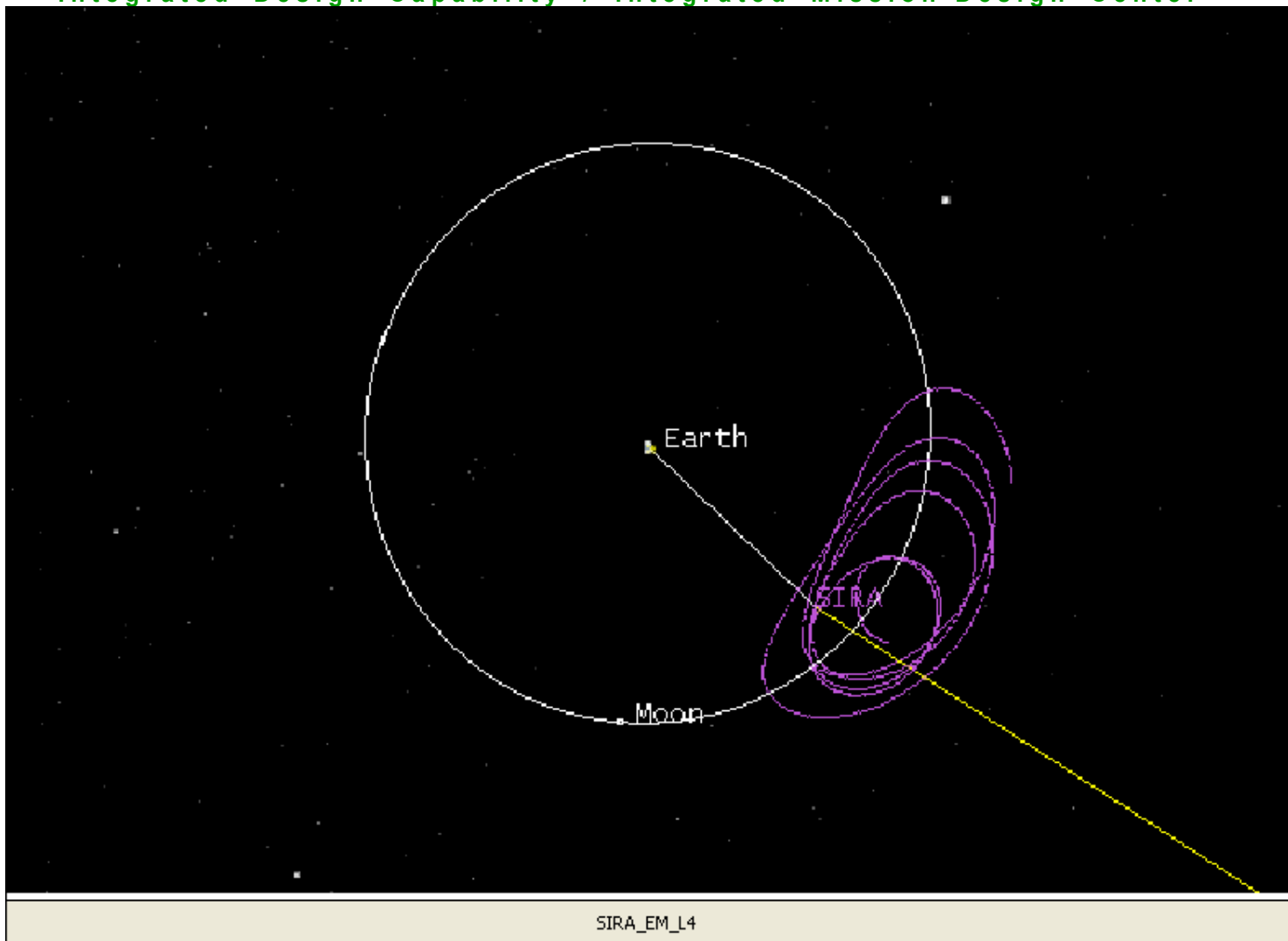
Shown in Earth-Moon Rotating System





Earth - Moon L4 Libration Orbit

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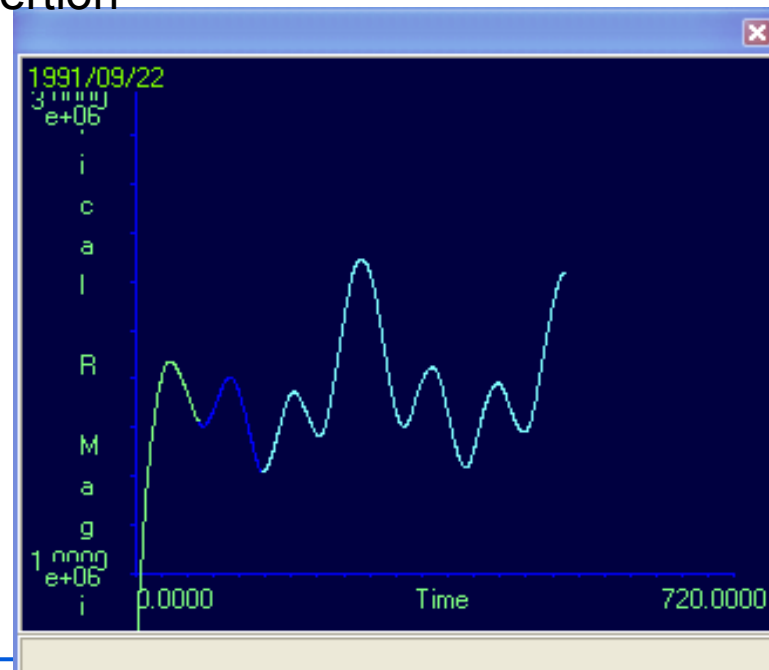
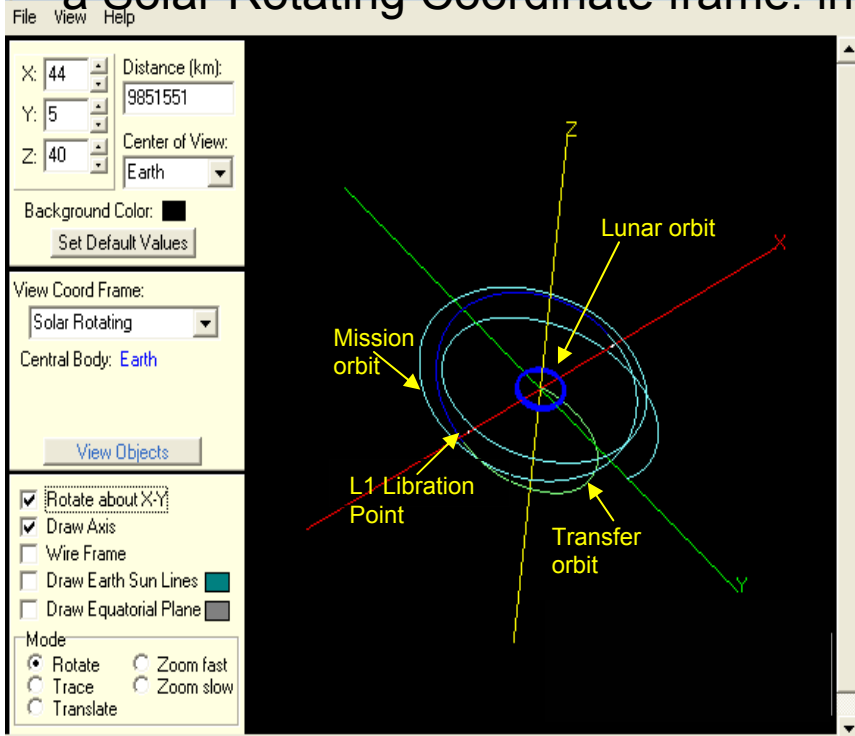


Distant Retrograde Orbit (DRO) Orbit

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- DRO is really an orbit in heliocentric space
- Heliocentric orbit parameters chosen that have same period of Earth with slightly altered eccentricity
- Circular relative motion wrt Earth orbiting clockwise
- Needs an insertion maneuver, but is stable afterwards
- It has dimensions of $\sim 1.7e6$ km in x and $<2.0e6$ km in y directions as measured in

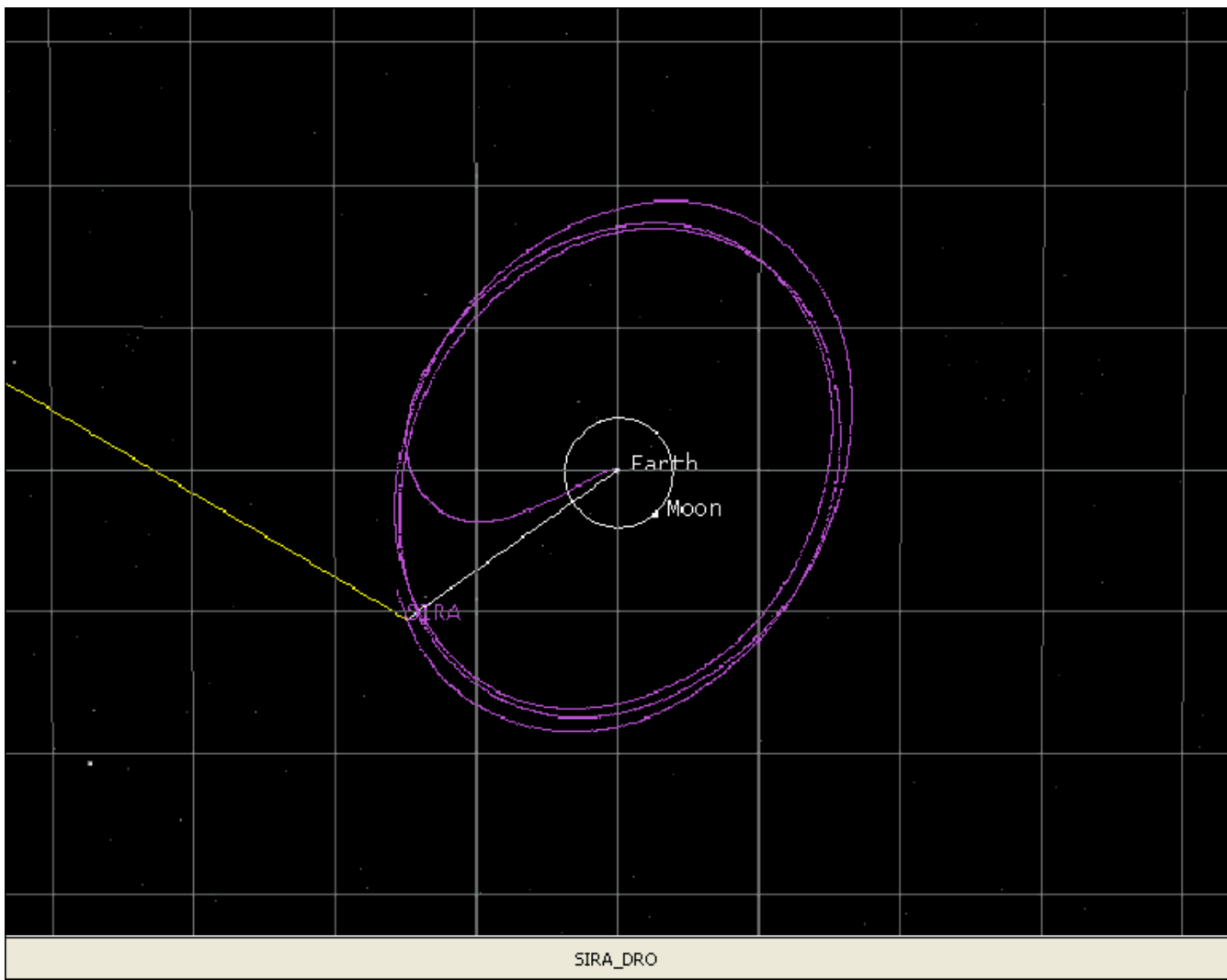
a Solar Rotating Coordinate frame: Insertion





Earth Distant Retrograde Orbit (DRO) Orbit

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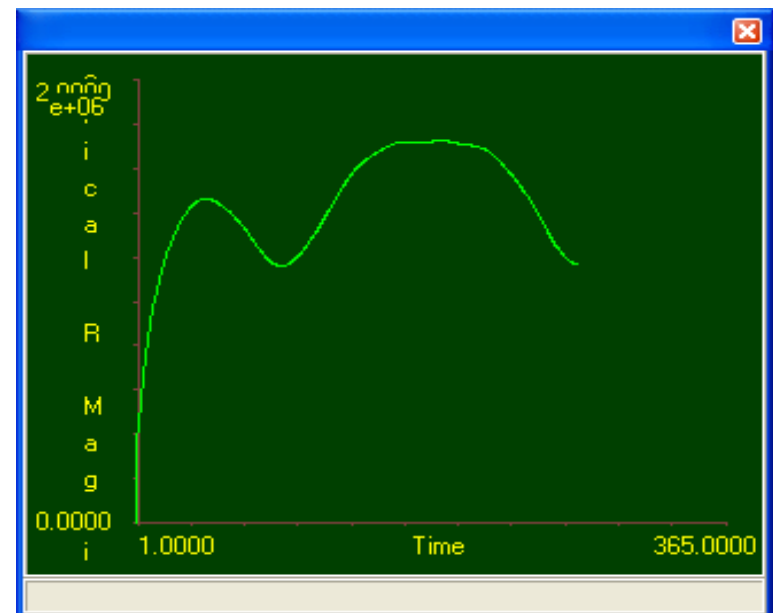
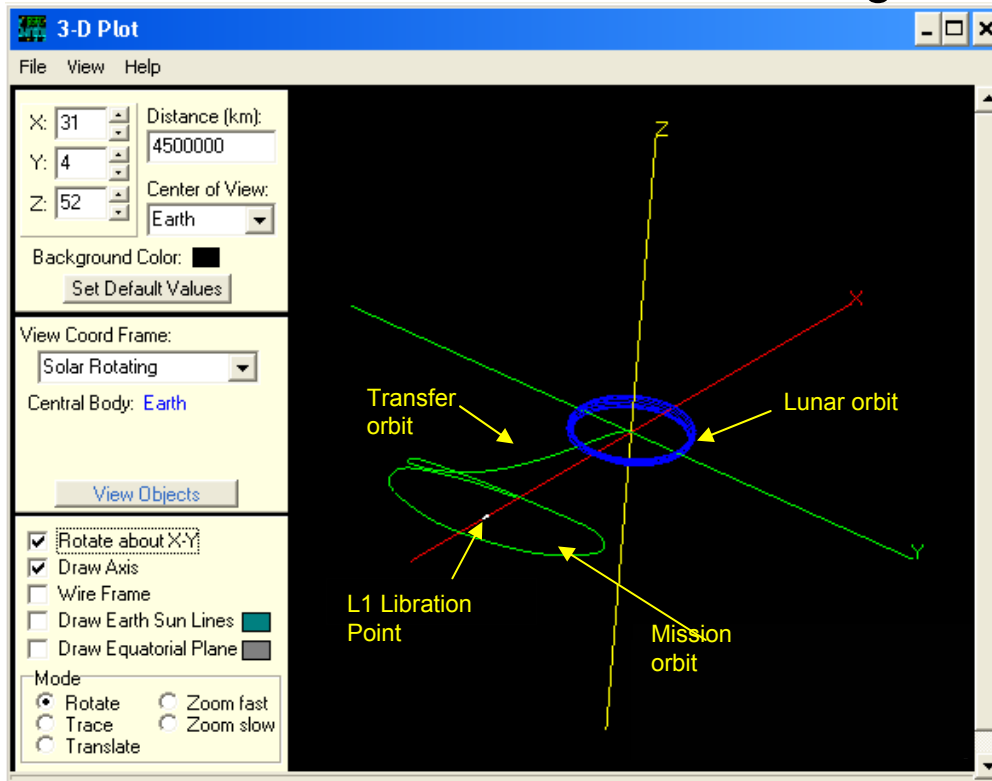




Libration Orbit

Integrated Design Capability / Integrated Mission Design Center

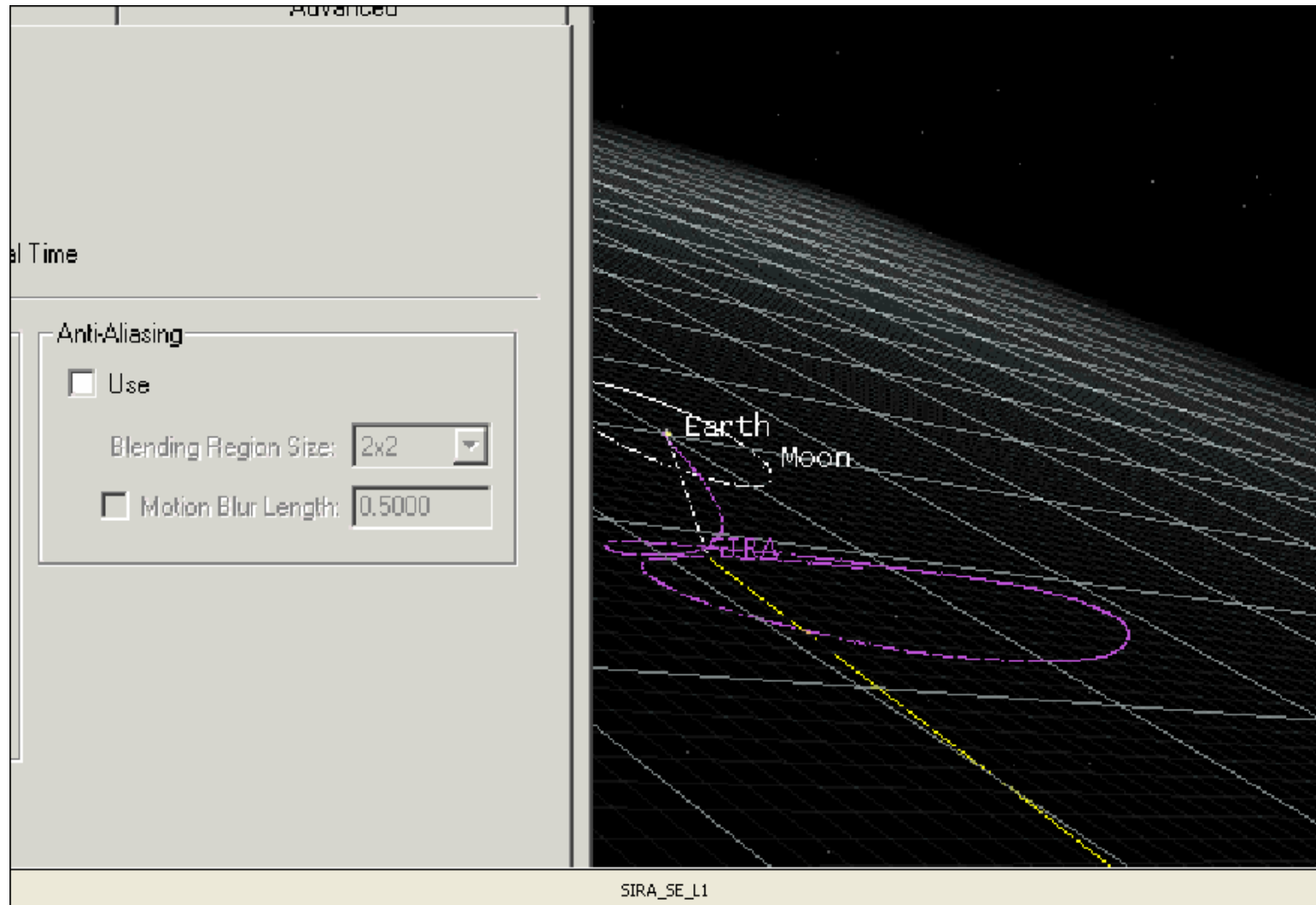
- This is a standard libration orbit about the co-linear L1 location (ISEE, SOHO, ACE)
- It has dimensions of about $1.6e6$ km in 'x' and $1.9e6$ km in 'y' directions as measured in a Solar Rotating Coordinate frame.





Libration Orbit

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Launch Vehicle Information

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- Corresponds to a C3 of $-0.5 \text{ km}^2/\text{s}^2$
- Mass to orbit ranges from 250 kg (Taurus) to 1510kg (Delta-III)

NASA Kennedy Space Center Expendable Launch Vehicles Flight Design Group

Vehicle Selection:

Plot Curve (5 Max)	Vehicle	Max Payload (kg)
<input type="checkbox"/>	Taurus (2230)	250.0
<input type="checkbox"/>	Taurus (2130)	295.0
<input type="checkbox"/>	Delta II (2326-10)	610.0
<input type="checkbox"/>	Delta II (2920-10L)	630.0
<input type="checkbox"/>	Delta II (2326-9.5)	635.0
<input type="checkbox"/>	Delta II (2920-10)	635.0
<input type="checkbox"/>	Delta II (2426-10)	700.0
<input type="checkbox"/>	Delta II (2920-9.5)	705.0
<input type="checkbox"/>	Delta II (2426-9.5)	720.0
<input type="checkbox"/>	Delta II (2425-10)	795.0
<input type="checkbox"/>	Delta II (2425-9.5)	820.0
<input type="checkbox"/>	Delta II (2920H-10L)	880.0
<input type="checkbox"/>	Delta II (2920H-10)	890.0
<input type="checkbox"/>	Delta II (2920H-9.5)	920.0
<input type="checkbox"/>	Delta II (2926-10L)	1085.0
<input type="checkbox"/>	Delta II (2926-10)	1095.0

Flight Design Group

Web Site	Vehicle	Max Payload (kg)
<input type="checkbox"/>	Delta II (2925-10L)	1240.0
<input type="checkbox"/>	Delta II (2925-10)	1250.0
<input type="checkbox"/>	Delta II (2925-9.5)	1305.0
<input type="checkbox"/>	Delta II (2926H-10L)	1320.0
<input type="checkbox"/>	Delta II (2926H-10)	1330.0
<input type="checkbox"/>	Delta II (2926H-9.5)	1360.0
<input type="checkbox"/>	Delta II (2925H-10L)	1495.0
<input type="checkbox"/>	Delta II (2925H-10)	1510.0
<input type="checkbox"/>	Delta II (2925H-9.5)	1540.0
<input type="checkbox"/>	Delta III (3940-11)	2655.0
<input type="checkbox"/>	Atlas IIIB (SEC)	3005.0
<input type="checkbox"/>	Atlas IIIB (DEC)	3215.0





Launch Vehicle Information

Corresponds to a C3 of $-1.8 \text{ km}^2/\text{s}^2$

- Mass to orbit ranges from 260 kg (Taurus) to 1585kg (Delta-III)

NASA Kennedy Space Center Expendable Launch Vehicles
Flight Design Group

<input type="checkbox"/> (to MAX)		
<input type="checkbox"/>	Taurus (2230)	260.0
<input type="checkbox"/>	Taurus (2130)	310.0
<input type="checkbox"/>	Delta II (2326-10)	625.0
<input type="checkbox"/>	Delta II (2326-9.5)	655.0
<input type="checkbox"/>	Delta II (2920-10L)	670.0
<input type="checkbox"/>	Delta II (2920-10)	675.0
<input type="checkbox"/>	Delta II (2426-10)	725.0
<input type="checkbox"/>	Delta II (2426-9.5)	745.0
<input type="checkbox"/>	Delta II (2920-9.5)	745.0
<input type="checkbox"/>	Delta II (2425-10)	820.0
<input type="checkbox"/>	Delta II (2425-9.5)	845.0
<input type="checkbox"/>	Delta II (2920H-10L)	925.0
<input type="checkbox"/>	Delta II (2920H-10)	935.0
<input type="checkbox"/>	Delta II (2920H-9.5)	965.0
<input type="checkbox"/>	Delta II (2926-10L)	1120.0
<input type="checkbox"/>	Delta II (2926-10)	1130.0
<input type="checkbox"/>	Delta II (2926-9.5)	1190.0

<input type="checkbox"/>	Delta II (2925-10L)	1275.0
<input type="checkbox"/>	Delta II (2925-10)	1285.0
<input type="checkbox"/>	Delta II (2925-9.5)	1340.0
<input type="checkbox"/>	Delta II (2926H-10L)	1360.0
<input type="checkbox"/>	Delta II (2926H-10)	1375.0
<input type="checkbox"/>	Delta II (2926H-9.5)	1400.0
<input type="checkbox"/>	Delta II (2925H-10L)	1535.0
<input type="checkbox"/>	Delta II (2925H-10)	1555.0
<input type="checkbox"/>	Delta II (2925H-9.5)	1585.0
<input type="checkbox"/>	Delta III (3940-11)	2730.0
<input type="checkbox"/>	Atlas IIIB (SEC)	3075.0
<input type="checkbox"/>	Atlas IIIB (DEC)	3300.0





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FreeFlyer Mission 5.3

File Run Edit Utilities Options Window Help

Run Duration: 27 Seconds

3D View

Jan 02 2005 02:19:27.965
Target: A1
Source: A1 (270° RA, 10° Dec, 600 km (radius))
FOV: 25°

Display

20 240 10

Plot

FreeFlyer Plot Window
1/30/2003

Formation.Range (km) Formation.Range (km) Formation.Range (km) Formation.Range (km)

A1.ElapsedDays (Days)	Formation.Range (km)
0.00	0
0.05	50
0.10	50
0.20	50
0.30	50
0.40	50
0.50	50
0.55	50

Plot

FreeFlyer Plot Window
1/30/2003

Formation.Mass (kg) Formation.Mass (kg) Formation.Mass (kg)

A1.ElapsedDays (Days)	Formation.Mass (kg)
0.00	25.0
0.05	24.2
0.10	24.2
0.20	24.2
0.30	24.2
0.40	24.2
0.50	24.2
0.65	24.2

Status Messages: Resume to continue, Terminate to end

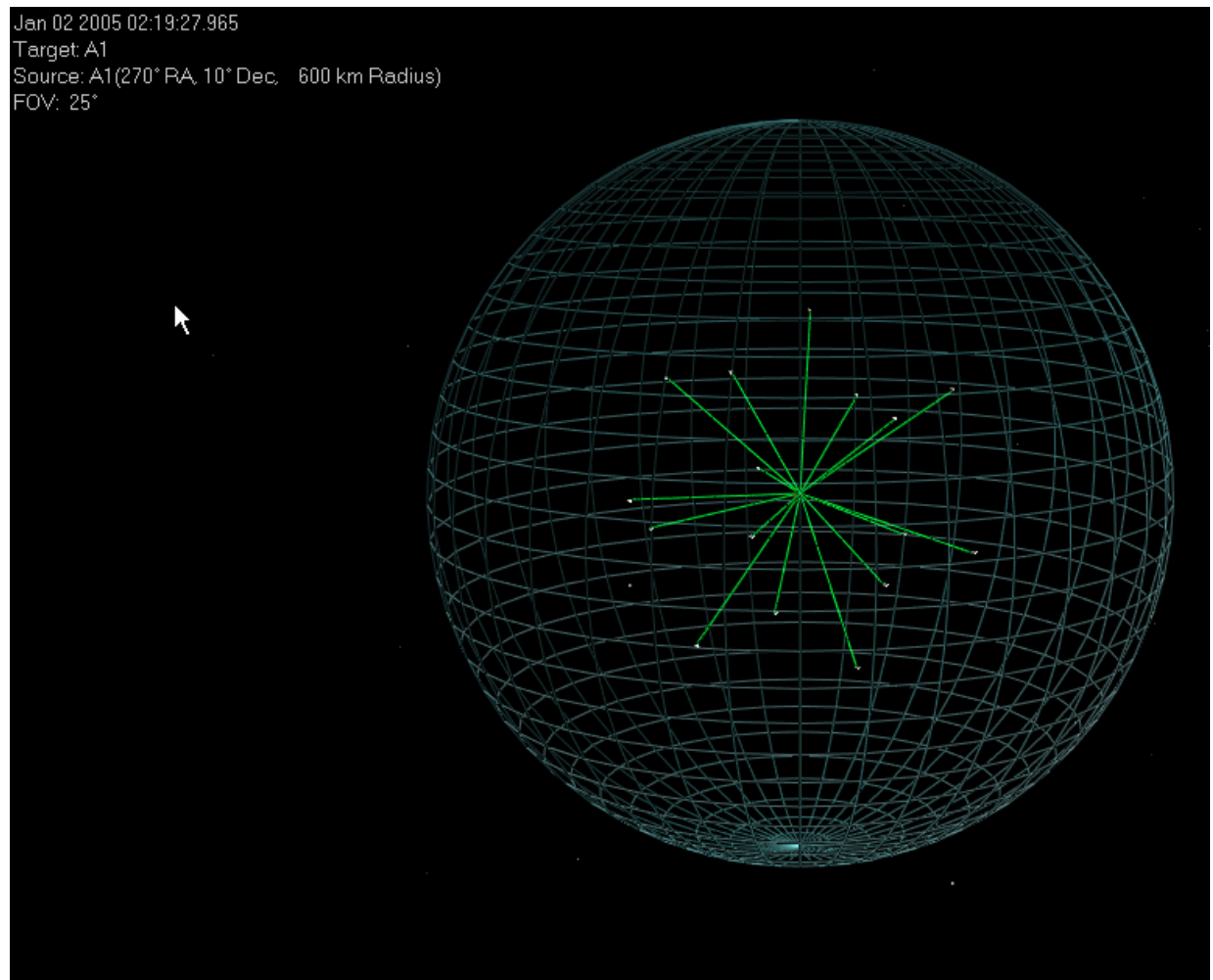
NORMAL MODE

Captured by Snagit
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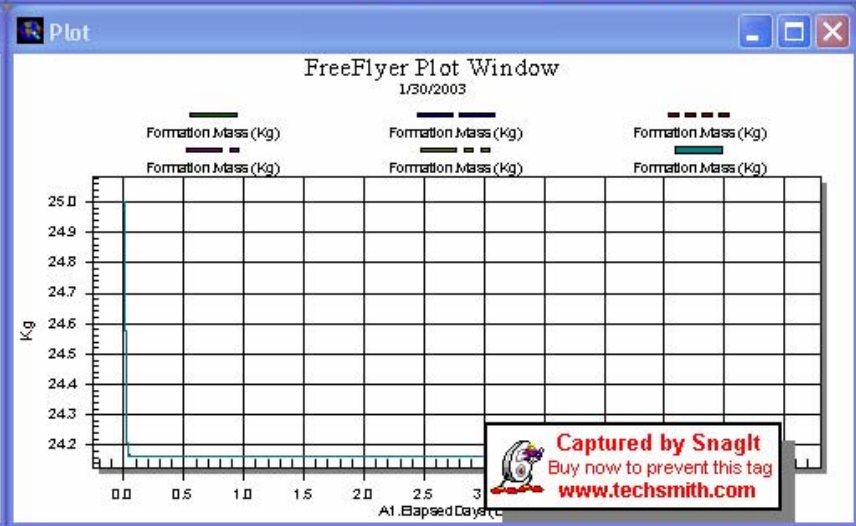
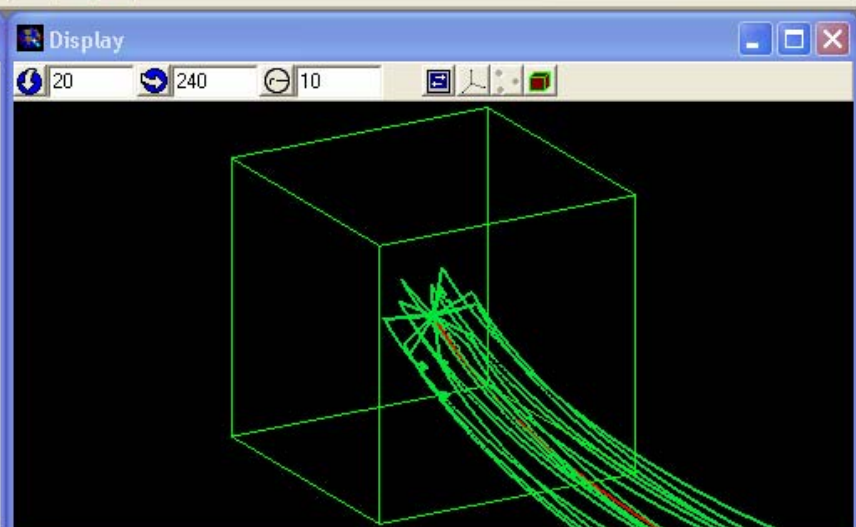
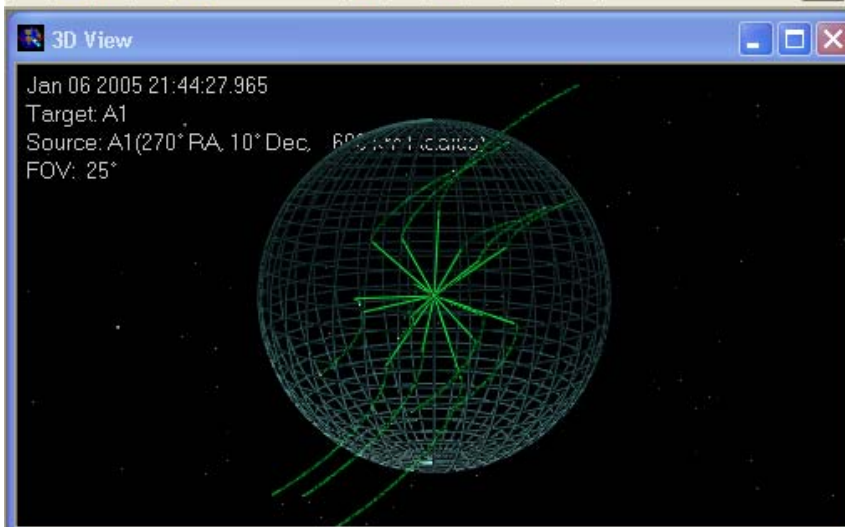




FreeFlyer Mission 5.3

File Run Edit Utilities Options Window Help

Run Duration: 39 Seconds



Status Messages | Resume to continue, Terminate to end | NORMAL MODE

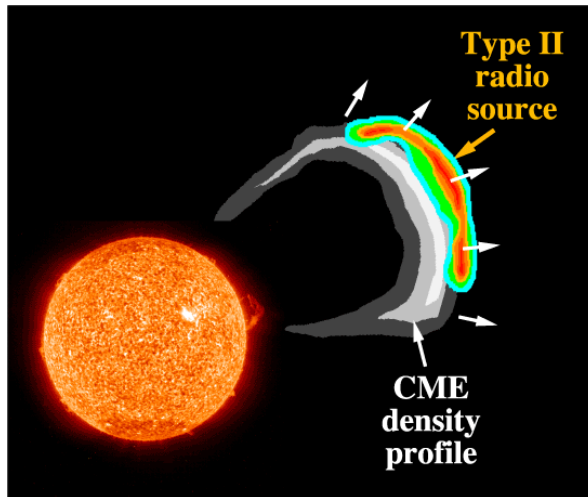
 **Captured by Snagit**
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Solar Imaging Radio Array

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Two dimensional radio imaging of the CME-driven shock front and the CME density profile is critical for predicting the space weather effects of CMEs

Technology Requirements:

- Intermicrosat ranging (to ~3 m)
- “Full-sky” aperture synthesis mapping algorithm development
- Onboard data cross-correlation desirable (for space weather snapshots)

Science Objectives:

- Understand CME structure, propagation, and evolution from the Sun to 1 AU
- Apply solar radio burst images to mapping of solar wind density structures and magnetic field topology, providing a unique tool for solar wind analysis
- Enhance space weather prediction capabilities using radio images of CMEs
- Observe and analyze the global response of Earth’s magnetosphere to CMEs and other space-weather-effective events from an external perspective
- Image the low-frequency (< 30 MHz) radio universe at high angular resolution and catalog and understand the objects found therein

Mission Description:

- Microsat constellation of 10 – 16 identical spacecraft
- Crossed dipole antennas and low frequency radio receivers
- Quasi-spherical constellation with <100 km diameter
- Nearly circular distant retrograde orbit (~10⁶ km from Earth) or other terrestrial radio interference limiting orbit
- Individual microsat communication with ground stations

Measurement Strategies:

- High spatial and temporal resolution
- Frequency range from ~30 MHz to ~30 kHz
- Frequency spacing and time resolution optimized for solar burst analysis
- Rapid data processing for space weather prediction

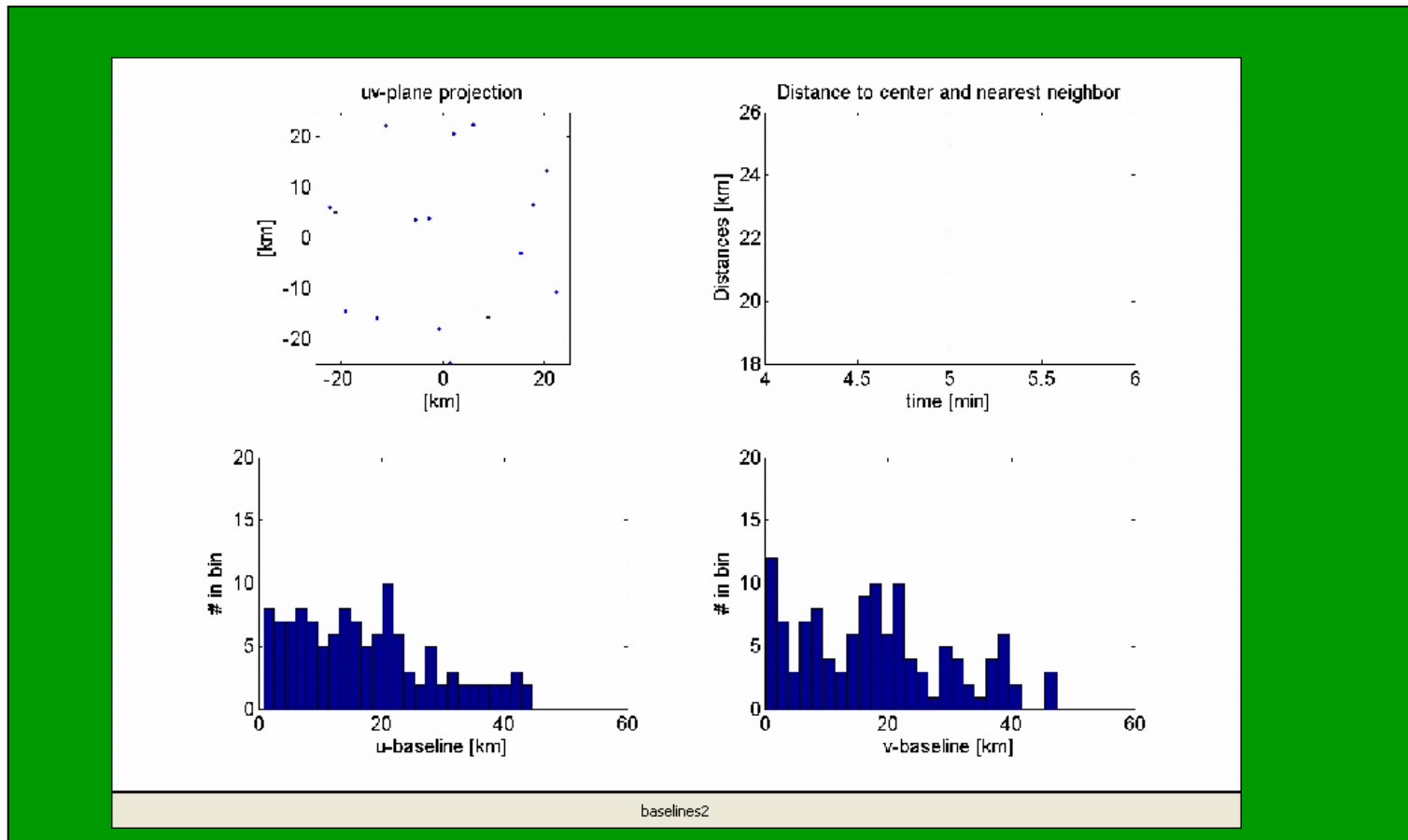




SIRA Formation U-V Plane Analysis

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- Spacecraft controlled to maintain only relative separations
- Plots show statistic of U-V plane and relative formation positions





Earth Distant Retrograde Orbit (DRO) Orbit

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SIRA Orbit Options – Lunar Transfer

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